



Non-linear Analysis of Slender High Strength Concrete Column

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Abstract

This article shows the influence of axial force eccentricity on high strength concrete columns design. The behavior of columns made of normal, middle and high strength concrete with slenderness values between 20 and 60 under an eccentric axial force has been studied. Structural analysis has been developed by means of software which considers both geometrical and mechanical non-linearity. The sequence of points defined by increasing values of axial force and bending moment produced by eccentricity has been represented on the cross-section interaction diagram until failure for each tested column. Then, diagrams depicting the relationship between failure axial force and column's slenderness have been drawn. The loss of bearing capacity of the member for normal and middle strength columns when compared with the bearing capacity of their cross-section is more noticeable as axial force eccentricity assumes higher values. However, this situation reverses for high strength columns with high slenderness values. On the basis of results obtained, the accuracy level for the moment magnifier method was checked. Despite the good concordance in most of the cases, it was verified that the moment magnifier method leads to excessively tight results for high strength concrete columns with high slenderness values. In these specific cases, a coefficient which amends the column rigidity is proposed so as to obtain safer values.

Keywords: Columns; Axial Force; High Strength Concrete; Non-linear Analysis; Moment Magnifier Method.

1. Introduction

Reinforced concrete rigid frames are the most widely employed structural system. They are composed by columns and beams. Columns are the structural elements whose prevailing internal force is an axial load which can be combined with one or two bending moments around two orthogonal axis.

Since the mid-twentieth century they have been targeted in many researches whose results, after being contrasted with pilot testing, have led to several calculation methods. In the case of short columns whose strength depends only on the bearing capacity of their section, we should mention the method proposed by Bresler [1] and more recently Hsu [2].

Gradual technological development has enabled the production of concretes with a higher strength to compression stress. The use of columns made of high strength concrete (HSC) in high-rise buildings reduces their section and increases the available space around them. The reduction of the cross section caused by the use of high strength concrete leads to slender columns whose bearing capacity is basically conditioned by their length. Therefore, a thorough analysis of second order effects derived from both the P- δ effect and the materials mechanic non-linearity is required.

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In order to know the first and more interesting theoretical and experimental studies about slender reinforced concrete columns, we can consult those done by Mavichak and Furlong [3] and Al-Noury and Chen [4]. However not only the concrete strength but also the slenderness values taken into consideration are the typical figures from those periods ($f_c < 50$ MPa and $\lambda < 50$), which are lightly smaller than those reached nowadays.

Studies about slender reinforced concrete columns made of HSC are much more recent but less often. Kim and Yang brought forth an experimental study with columns whose involved variables were slenderness, concrete strength and steel ratio [5]. Nevertheless, the axial force was applied with the same eccentricity on the pillar in all the cases tested.

Interest in a deeper knowledge on the behavior of these complex structural elements has currently increased. Recently lab tests have been carried out not only on NSC slender columns [6] but also on HSC short [7] and slender columns [8, 9]. Results of work of Barrera et al. [10] confirm that reduced axial load decreases for an increase of the concrete strength and slenderness of the specimen. However, in this research axial force is always applied with different eccentricity values on both bar ends.

Thus, the main objective of this article consists of researching the effect of the axial force eccentricity on the bearing capacity reduction because of second order effects on slender columns made of low, medium and high strength concretes.

Results obtained have been compared with those from the application of the well-known moment magnifier method contained in the ACI 318 [11] in order to determine its safety level. This method, when employed for NSC columns, provides unsafe values in one of the laboratory tests (test S10-A1) carried out by Leite et al. [12]. This author points in his conclusions that the accuracy of this method in HSC columns is lower than in NSC columns.

This work will widen our knowledge on this subject by taking into consideration columns with usual heights in architectural building and by considering an axial force applied with the same eccentricity on both sides of the column. It will also verify the accuracy of the moment magnifier method for HSC slender columns.

Structural analysis has been addressed with matrix stiffness method software which takes into account the second order effects produced by not only the interaction between axial force and lateral displacements but also the materials non-linear behavior. Loads application has been done in an incremental way following the procedure described by McGuire [13].

Final results will help us to understand the behavior of such a complex structural element under several load scenarios.

2. Computer Assisted Testing Software

Complexity and high economical cost of laboratory tests on actual columns make them rather difficult. Alternatively, several analytical methods so as to determine the failure load values for NSC and HSC columns can be employed. Some of the most recent ones are those published by Agha and Rashid [14] and Abdel-Karim et al. [15]. Also, it is possible to analyze a vast range of models in a reduced amount of time by means of advanced software which reproduces perfectly the columns non-linear behavior [16]. The software and the assumptions used are described hereunder.

2.1. Assumptions

The calculation process assumes the ensuing hypothesis:

- Plane cross sections strain remains plane (Navier's Hypothesis). Hence strains are proportional to the distance to the neutral axis.
- There is deformational compatibility between steel and concrete along their contact surfaces.
- Concrete's shrinkage and creep effects and concrete's tension strength are not to be taken into account.
- Shear stresses effects are disregarded

2.2. Constitutive Equations for Materials

Non-linear structural design equation suggested by Eurocode 2 [17] has been employed in the case of concrete (Figure 1.a). Relationship between stresses and strains can be expressed by means of function (Equation 1):

$$\frac{\sigma_c}{f_{cm}} = \frac{\kappa \cdot \eta - \eta^2}{1 + (\kappa - 2) \eta} \quad (1)$$

Where

$$f_{cm} = f_{ck} + 8 \quad (2)$$

$$\eta = \epsilon_c / \epsilon_{cl} \tag{3}$$

$$\epsilon_{cl} = 0.7 \cdot f_{cm}^{0.31} \leq 2.8 \tag{4}$$

$$\kappa = (1.05 \cdot E_{c, nom}) \cdot \epsilon_{cl} / f_{cm} \tag{5}$$

$$E_{cm} = 22 \cdot [(f_{cm}) / 10]^{0.3} \tag{6}$$

$$\epsilon_{cu} = 2.8 + 27 \cdot [(98 - f_{cm}) / 100]^4 \tag{7}$$

As for rebars steel and according to Eurocode 2, a simplified stress-strain diagram constituted by just two branches is employed (Figure 1.b). First branch arises from the origin with a slope whose value is E_s until the characteristic yield point of steel (f_{yk}) removal is reached. Second branch is to be considered horizontal, until the ultimate strain with a value of $\epsilon_{u} = 0.01$ is reached.

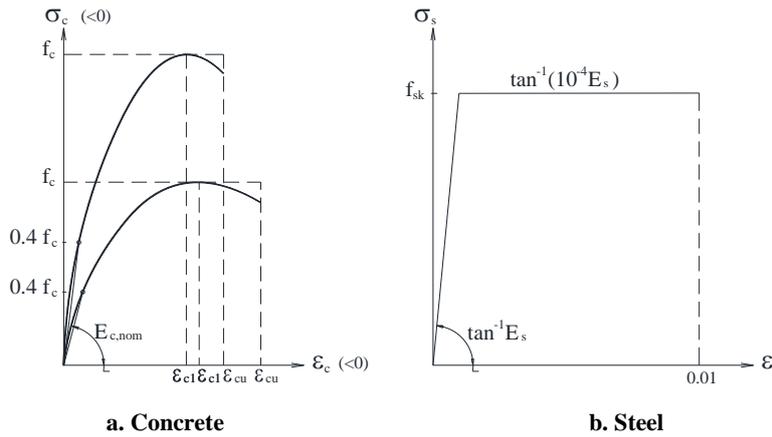


Figure 1. Stress-strain diagrams

2.3. Structural Analysis for Columns

A reinforced concrete column bearing capacity is usually represented by means of interaction diagrams $P-M$. They consist of the values of axial force (P) and bending moment (M) which produce the cross-section failure when being applied simultaneously. Considering a linear behavior for the column, the load trajectory would be a line until failure is reached (point A on the interaction diagram).

As for slender columns, this trajectory is a curve as long as second-order effects cannot be disregarded. Nonlinear behavior of materials and the additional internal forces produced by the axial force being applied on geometry with lateral deformations which cannot be dismissed ($P-\delta$ effect) produce a higher increase of bending moments which reduce the ultimate load value.

Failure of the bar can occur in two different ways. Load trajectory can reach the interaction diagram, collapsing because of strength failure. However, regarding very slender columns, collapse may happen because of instability, so the load trajectory never can reach the interaction diagram (Figure 2).

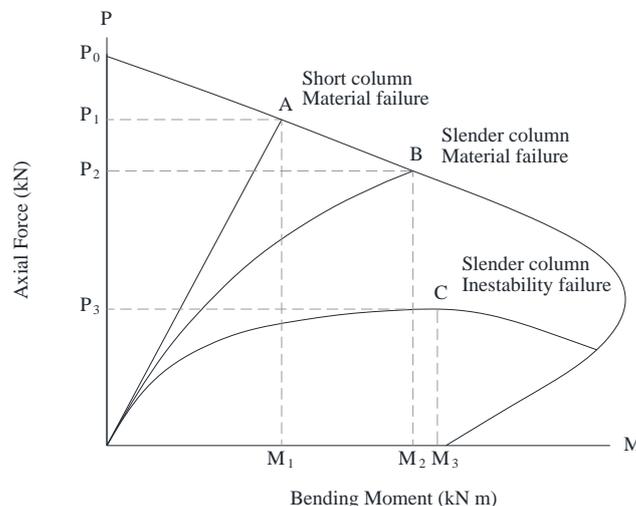


Figure 2. Path of axial force / Bending moment values until failure of slender columns

Most of the reinforced concrete columns employed in building structures collapse because of strength failure as long as slenderness ratios are lower than the critical values which produce instability [18, 19]. But nowadays the employment of high strength concrete in building structures enables smaller cross sections for the columns. That means higher slenderness values and makes more likely the chance of failure because of instability.

Structural analysis was developed by means of non-linear calculation software named ANGLE [20]. According to the method proposed for Wang and Hsu [21], the beam-column geometrical model defined by the different bars directrix was discretized a series of bar stretches whose nodes initial coordinates were obtained. Axial force with a pre-established eccentricity was applied progressively in several load stages until the bar failure.

Geometrical non-linearity has been taken into account at each stage by considering in the stiffness matrix the deformed geometry corresponding to the previous stage. The process looking for the structure's balance within the different load stages was developed by means of the Newton-Raphson method.

Mechanical non-linearity has its influence on the stiffness modulus ($E \cdot I$) to be considered in the stiffness matrix. Because of the different materials non-linear behavior its determination requires applying some iterative process in order to find the cross-section equilibrium. Within this work the procedure developed by Fenolosa et al. [22] has been used. It consists of two linked loops. First one locates the strains plane curvature by means of axial forces balance. Second one locates neutral axis by bending moments balance. Once the cross-section equilibrium was achieved, stiffness modulus was deduced helped by the expression $E \cdot I = M / \phi$.

2.4. Geometry and Configuration

Thirty-six different models for columns with square-shaped cross section measuring 45×45 cm and reinforced with 8 bars with a diameter of 20 mm placed in the corners with a reinforcement mechanical cover of 40 mm have been tested (Figure 3 left). Rebars amount implies a relation $\rho = 1.256\%$ in relation to the concrete area.

Tested bars lengths are comprised between 3 and 8 meters. That includes the usual height that can be found in building structures. They were modelled with pin joints at both ends and without taking into account any potential directrix imperfections (Figure 3 right).

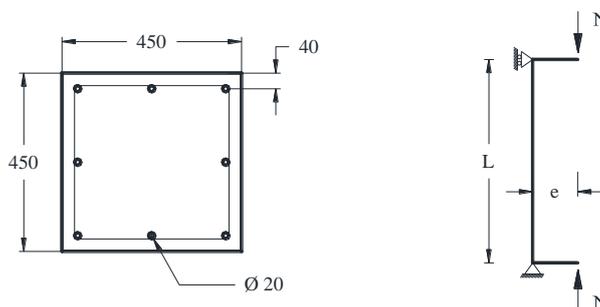


Figure 3. Analyzed columns cross section and loads application model

Bars mechanical slenderness has been defined by the equation $\lambda = l_0 / i$ and ranges between 20 and 60, being 10 the effective buckling length and i the bending radius for the gross section without taking cracking into account.

Two different eccentricities, with regard to the cross-section center of mass when applying the axial force, have been considered: 20 and 100 mm.

Regarding concrete, three different strengths have been employed: 30 MPa for normal strength concrete (NSC), 60 MPa for middle strength concrete (MSC) and 90 MPa for high strength concrete (HSC). The characteristic values for the three different types of concrete within this work are collected in Table 1.

Table 1. Characteristic values for concrete

f_c (MPa)	f_{cm} (MPa)	E_{cm} (MPa)	ϵ_{c1}	ϵ_{c2}
30	38	33.000	0.0022	0.0035
60	68	39.000	0.0026	0.0030
90	98	44.000	0.0028	0.0028

Steel, with a yield strength value of 500 MPa, a failure strain value of $\epsilon_{st} = 0.01$ and a modulus of elasticity value of $E_s = 210.000$ MPa, was employed.

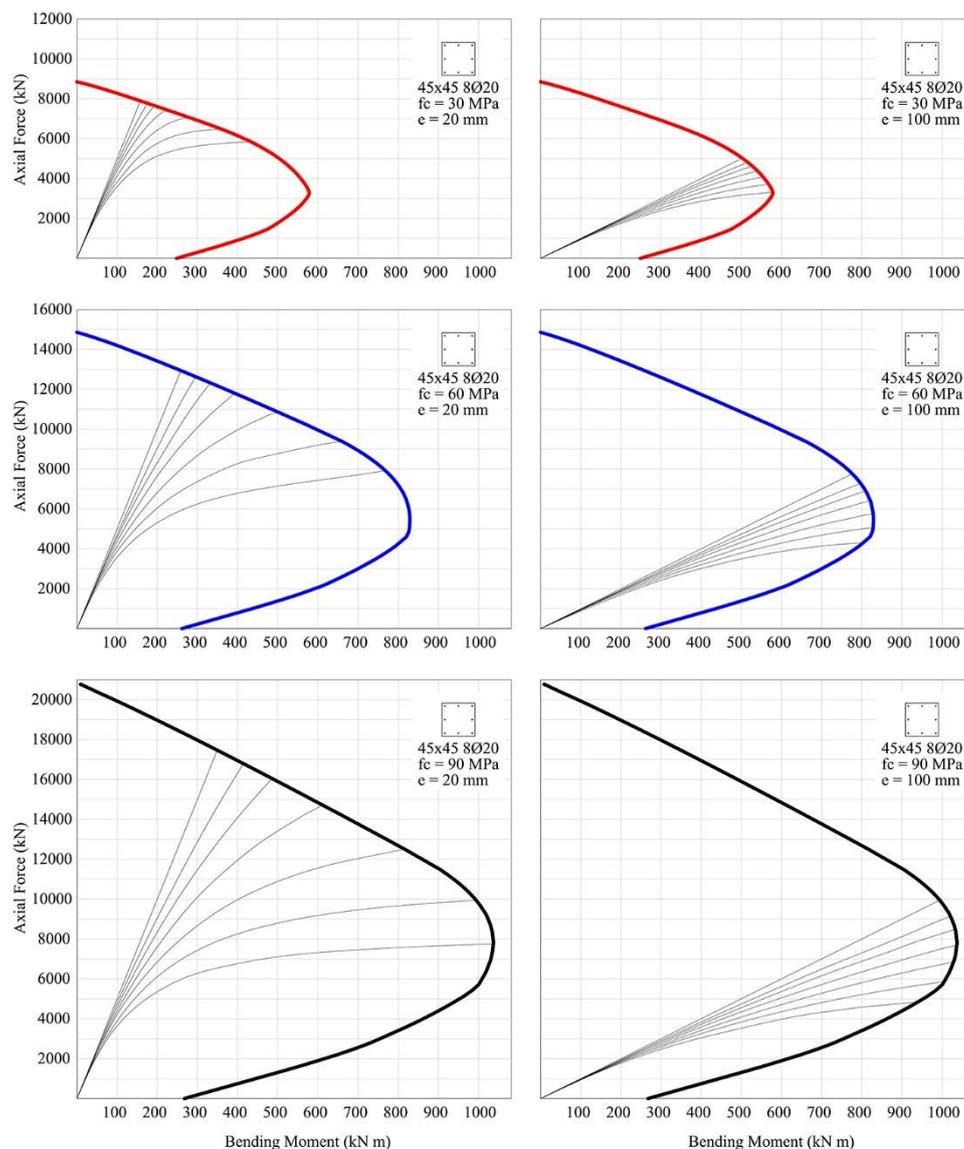
These parameters were taken into consideration when applying the materials constitutive equations, not only for the determination of the stress value at each fiber when a certain strain is imposed, but also for introducing the failure criterion when the ultimate strain has been reached.

3. Structural Analysis Results

Non-linear structural analysis for different columns has been carried out by means of the described mathematical model. The path of the axial force and bending moment values until failure for each tested column has been represented on the cross-section interaction diagram (Figure 4).

Considering the same slenderness value, it can be observed that the higher strength for the concrete, the more horizontal shape for the final stretch of the axial force and bending moment diagram. Despite this fact is produced with both analyzed eccentricities, it is more obvious for the 20 mm one. Path's horizontality means that the column instability failure is more likely and it increases as the column slenderness and concrete's strength increase.

Regarding high slenderness values ($\lambda=60$), ultimate axial force value for middle strength concretes is similar to the figure obtained for high strength ones. That is more often in the case of small eccentricity when applying the axial force.



a. Axial force eccentricity=20 mm

b. Axial force eccentricity=100 mm

Figure 4. Axial force - Bending moment interaction diagrams

Knowing the previous values diagrams relating the axial force value and column's slenderness for different types of concrete for the two above mentioned axial force eccentricities have been elaborated (Figure 5). That illustrates the influence of the slenderness of the member on its bearing capacity reduction.

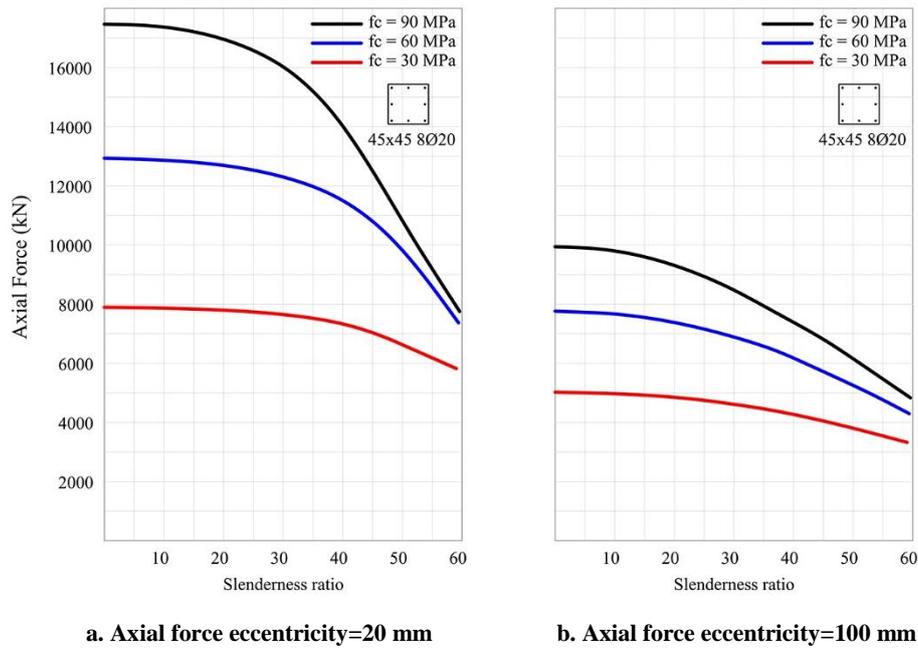


Figure 5. Ultimate load - Slenderness ratio diagrams

It can be observed that the loss of bearing capacity is bigger in columns made of high strength concrete as highlighted by Kim and Yang [5] y Leite et al. [12]. Its efficacy decreases especially for very slender columns, for which the load capacity tends to converge. That fact is especially obvious in curves for HSC and MSC columns when the load is applied with an eccentricity of 20 mm (Figure 5.a). For slenderness values over 60, ultimate load for HSC columns is similar than the one for MSC columns for both eccentricities (Figure 5.a and 5.b). This is caused by the greater fragility akin to this type of concretes.

In order to understand the behavior of high strength concrete columns, it is very interesting to represent the bearing capacity reduction in a non-dimensional way (Figure 6).

The hereunder diagrams represent the relationship between the column ultimate load and the section ultimate load (P_u/P_n) with respect to the slenderness for the three different types of concrete employed and for both eccentricities analyzed.

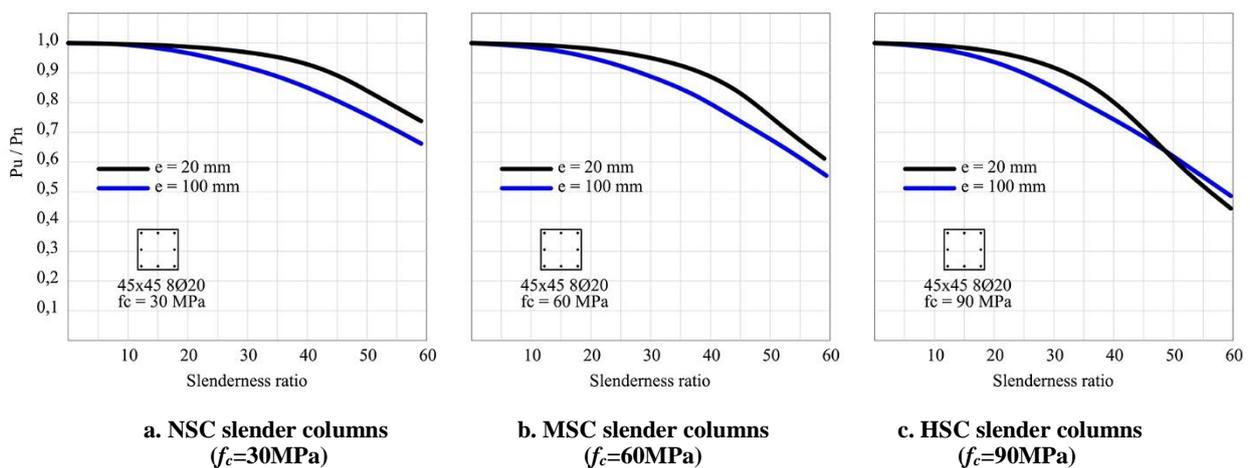


Figure 6. P_u/P_n - Slenderness ratio diagram of beam-columns

The column bearing capacity, when compared with the cross-section ultimate load, decreases faster for higher values of concrete strength and/or for higher values of slenderness of the member, for both analyzed axial force application eccentricities. That means that HSC columns are, in comparison, less efficient especially as bar slenderness values increase.

In the analyzed case, the loss of bearing capacities in normal and middle strength increases with the axial force application eccentricity. As for NSC, both eccentricities curves are lightly parallel with slenderness values higher than 30. As for MSC, the maximum difference is reached with a slenderness value of 40 and then there is a light tendency to converge (Figure 6.b). As for HSC, curves cross when the bar slenderness approaches 50 (Figure 6.c). That means that

for small and medium slenderness values, the loss of bearing capacity is higher for a higher eccentricity value, whilst for high slenderness values the situation is reversed.

From the obtained results we can deduce that HSC loses most of its efficacy as the column slenderness values increases, especially in the case of rather centered axial force application.

4. Moment Magnifier Method

4.1. Method Description

There are simplified design methods which can be employed as an alternative to the non-linear analysis exposed by Eurocode 2 as a general design method. Among them, we can find the one suggested by Kwak and Kim [23] based on a strength reduction coefficient application or the very simple moment magnifier method recommended by ACI 318 [11]. Following its instructions, beam column failure forces can be deduced from a first-order elastic calculation ($P_u M_u$). Values for the column design taking into account second-order effects ($P_u \delta M_u$) have been obtained by amplifying the bending moment value with a magnification factor to be quantified by means of the ensuing equation (Equation 8):

$$\delta = \frac{C_m}{1 - P_u / \phi \cdot P_{cr}} \geq 1 \quad (8)$$

Where

C_m is a coefficient which takes into consideration the axial force eccentricity applied on both ends. In this case, eccentricity value is the same on both ends so a value of $C_m=1$ was adopted.

ϕ is a bearing capacity reduction coefficient. So as to assess the total bearing capacity, a value of $\phi=1$ was accepted.

P_{cr} is the Euler buckling load determined by Equation 9:

$$P_{cr} = \frac{\pi^2 \cdot EI}{(k \cdot l_o)^2} \quad (9)$$

Where

k is a coefficient which takes into account the link conditions in both ends of the bar.

l_o is the length of a bar with pin joints on both ends.

$E \cdot I$ is the flexural rigidity of the column cross-section. This is the main factor in the evaluation of the bearing capacity of the supports. Its correct estimate is subject of continuous research [24, 25, 26, 27]. ACI 318 sets out two different equations for determining flexural rigidity. This study has chosen the following one:

$$E \cdot I = \frac{0,4 \cdot E_c \cdot I_g}{1 + \beta_d} \quad (10)$$

Where

E_c is the concrete elastic modulus of concrete. During this research its value has been obtained by Equation 11. according to ACI 318.

$$E_c = 4700 \sqrt{f'_c} \quad (11)$$

I_g is the second moment of inertia of the concrete gross section.

β_d is the concrete creep factor. Since this work doesn't consider the concrete shrinkage effects, a value of $\beta_d=0$ was adopted.

The moment magnifier method was initially developed for NSC columns. Recent lab tests have shown a good correspondence for this type of columns, but not for HSC columns as long as obtained values are much more adjusted. It even provides unsafe values when slenderness and axial force eccentricity increase as it can be checked in tests S09-A1, S10-A1, S11-A1 and S12-A1 of the research carried out by Leite et al. [12].

4.2. Comparative Study Results

On the basis of the obtained values, Table 2 has been elaborated. It displays the ratio between the ultimate axial force deduced with a non-linear calculation (P_u) and that one obtained with the moment magnifier method (P_{ACI}).

Despite the fact that there are other particulars which have not been taken into account within this work such as the proportion of longitudinal reinforcement bars or the relationship between the eccentricities of the axial forces applied

on both ends of the bar, values of P_u/P_{ACI} obtained are sufficiently close to those published by Mendis [28] and Leite et al. [12] in their comparative works which included lab tests.

Table 2. P_u/P_{ACI} ratio for NSC, MSC and HSC slender columns

	$f_c = 30 \text{ MPa}$		$f_c = 60 \text{ MPa}$		$f_c = 90 \text{ MPa}$	
	$e=20\text{mm}$	$e=100\text{mm}$	$e=20\text{mm}$	$e=100\text{mm}$	$e=20\text{mm}$	$e=100\text{mm}$
3 m	1,006	1,019	1,014	1,029	1,017	1,030
4 m	1,013	1,031	1,031	1,055	1,034	1,049
5 m	1,024	1,047	1,060	1,080	1,055	1,056
6 m	1,034	1,054	1,100	1,088	1,052	1,092
7 m	1,045	1,058	1,125	1,085	1,026	1,081
8 m	1,086	1,058	1,117	1,070	0,991	1,048

The diagrams of Figure 7 show, in a non-dimensional way (P_u/P_n), the bearing capacity reduction obtained by means of the explained procedure when compared with the results having applied the moment magnifier method. Axial force has been applied with an eccentricity of 20 mm in the three diagrams of the first row and with an eccentricity of 100 mm in the diagrams of the second row. Three different values of concrete strength have been employed respectively: 30, 60 and 90 MPa.

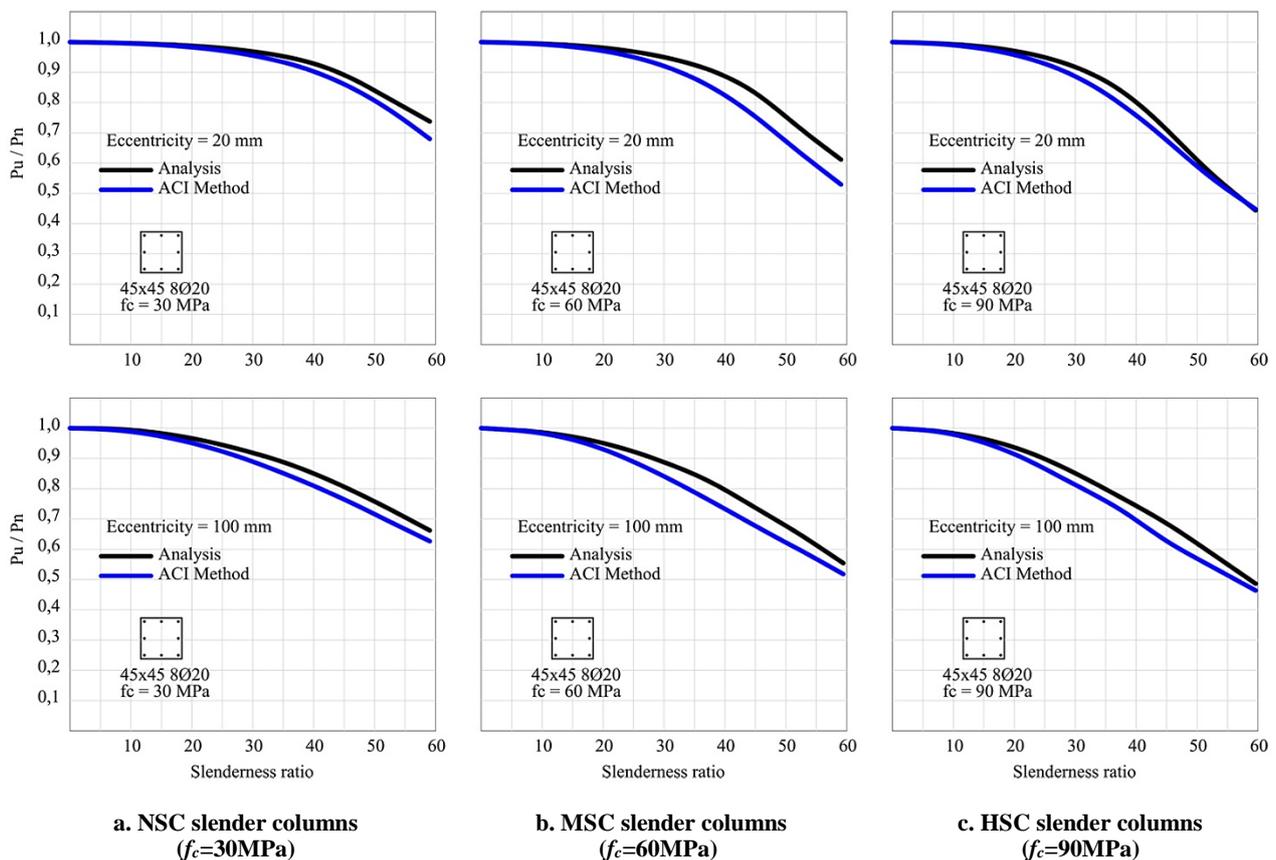


Figure 7. (P_u/P_n) - Slenderness comparative diagrams

On the whole, the moment magnifier method has a good concordance with the non-linear analysis model developed and the materials constitutive equations used.

Concordance is higher in the case of NSC columns for any eccentricity analyzed, supplying more conservative values in the case of MSC columns (Figure 7.a and 7.b). Nevertheless, in the case of HSC with axial force applied with an eccentricity of 20 mm, both diagrams intersect when slenderness value is about to reach 57 (Figure 7.c). Hence, the moment magnifier method can lead to unsafe values for higher slenderness values. Regarding the eccentricity value of 100 mm and despite lines never cross, it can be observed certain convergence between them. That induces the suspicion that, even for this eccentricity value, the moment magnifier method could provide excessively tight values for higher slenderness values.

It is understandable that a higher concordance with the moment magnifier method can be found in the case of NSC columns, meaning a sufficient safety margin, since this method was developed when the employ of concretes with this range of strength was usual. The direct application for HSC columns must be done carefully.

4.3. Flexural Rigidity Value Revision

The equation proposed by the ACI 318 to get the $E \cdot I$ term, was obtained for normal strength concrete. Bonet et al. [29] suggest its revision for application to HSC columns. The work of Lee et al. [30] shows that expressions for estimating the elastic modulus for concrete proposed by codes Eurocode 2 and ACI 318 provide higher values than those obtained by means of laboratory tests for middle and high strength concretes. Tikka and Mirza [31] suggest the use of alternative equation to the one proposed by ACI 318 in order to determine the value of EI . In that equation this value depends on the end eccentricity ratio (e/h) which means an EI value which is not only variable but also non-linear.

In order to obtain similar safety values in HSC columns than in NSC and MSC columns when the moment magnifier method is applied, an additional coefficient (γ) (Equations 12 and 13) is suggested. This one reduces the flexural rigidity for slenderness values higher than 50:

$$E \cdot I = \frac{0,4 \cdot E_c \cdot I_g}{1 + \beta_d} \cdot \gamma \quad (12)$$

Where:

$$\gamma = 1 - \frac{\lambda - 50}{4\lambda} \leq 1 \quad (13)$$

Diagrams in Figure 7 in the case of HSC columns have been remade applying the correction coefficient suggested by the authors when determining the bearing capacity of the column by means of the moment magnifier method. Non-dimensional diagrams depicted in Figure 8 show that the application of this coefficient in the case of HSC columns leads to safety levels for high slenderness values which are similar to those obtained for lower slenderness values.

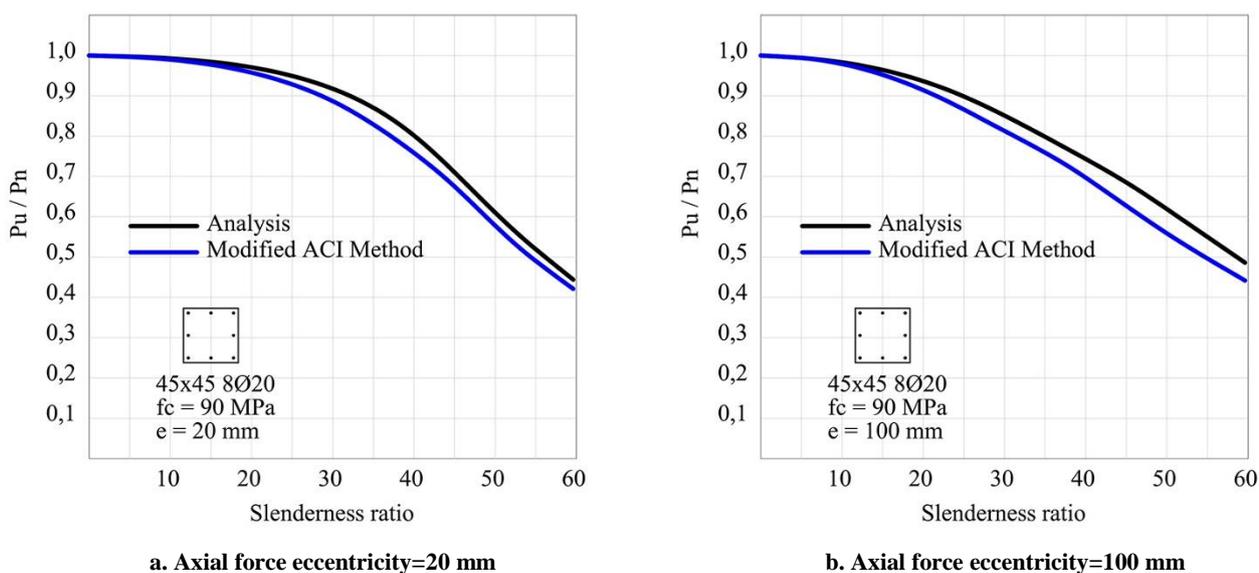


Figure 8. Modified (P_u/P_n) - Slenderness comparative diagrams for HSC columns

5. Conclusions

A procedure for obtaining the ultimate load for slender concrete columns taking into account the geometrical and mechanical non-linearity has been showed. This procedure has been developed for analyzing columns with different slenderness values and made of normal, middle and high strength concretes under axial force applied with two different eccentricities.

On the basis of the results, it can be concluded that:

- The loss of bearing capacity in columns because of second-order effects is higher in high strength concretes. Ultimate load values for very slender columns is just a little bit higher for HSC columns than it is for MSC (in the case of much centered axial forces and high slenderness values). This is because of the HSC concretes higher fragility. Hence, an efficient use of concrete considering strictly strength leads us to reconsider the use of HSC in

very slender columns ($\lambda > 50$). The work of Adinarayana and Ramudu provides a useful information about the effect of using HSC columns on the structural behaviour of buildings [32].

- Increasing the axial force eccentricity produces a higher loss of the bar bearing capacity when compared with the bearing capacity of the section. This phenomenon can be noticed for low or medium slenderness values in any sort of concretes. However, this situation reverses in HSC columns with high slenderness values (Figure 6.c).
- Thereupon, the use of high strength concrete for columns with high slenderness values is more effective when the axial force comes along strong transversal thrusts such as those produced by wind or earthquakes. And it is less effective in the case of strong gravity loads applied on the cross-section center of mass.
- In the case of NSC and MSC columns, the moment magnifier method included in the ACI regulations has a very good concordance with the laboratory tests and the analytical results exposed. However, it leads to excessively tight or even unsafe values in the case of very slender HSC columns. This work has suggested the application of a correction coefficient which reduces flexural rigidity and leads to more conservative values for this type of columns

6. Nomenclature

f_{ck}	Characteristic strength value for concrete;
f_{cm}	Compressive strength average value for concrete;
ε_{c1}	Concrete strain due to maximum stress;
ε_{cu1}	Ultimate concrete compressive strain;
f_{yk}	Characteristic strength value for steel;
ε_u	Ultimate steel compressive strain;
E_{cm}	Secant modulus of elasticity for concrete;
λ	Mechanical slenderness of the column;
C_m	Coefficient which takes into consideration the axial force eccentricity applied;
ϕ	Bearing capacity reduction coefficient;
P_{cr}	Euler buckling load;
K	Coefficient which takes into account the link conditions in both ends of the bar;
l_0	Length of a bar with pin joints on both ends;
I_g	Second moment of inertia of the concrete gross section;
i	Bending radius for the concrete gross section;
β_d	Concrete creep factor;
P_n	Ultimate load of the section;
P_u	Ultimate load of the column;
P_{ACI}	Ultimate load of the column in ACI method.

7. Funding

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8. Conflicts of Interest

The authors declare no conflict of interest.

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